Directional ground fault detection in resonant-grounded or isolated networks

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# SIPROTEC 5 Application

## Directional ground fault detection in resonant-grounded or isolated networks

APN-077, Edition 1.1, 12.03.2021

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1 Introduction

This application note provides information about:

- Directional ground fault detection in resonant-grounded or isolated networks
- Proposed standard functions to be applied, depending on network grounding, network structure and ground fault type
- Configuration recommendations for these functions
- Recommendations for threshold settings, explained by an application example
- General configuration recommendation (e.g., recording, avoiding signals floods in case of intermittent ground faults)
2 Overview about available functions ant their application

The following table provides an overview about which functions are applicable for

a. Different ground fault types: permanent, intermittent, transient
b. Network grounding: resonant, isolated
c. Network structure: radial, meshed / ring

<table>
<thead>
<tr>
<th>Function (block) type</th>
<th>Ground fault type</th>
<th>Network grounding</th>
<th>Network structure</th>
</tr>
</thead>
<tbody>
<tr>
<td>Dir. 3I0&gt; stage with cosφ measurement</td>
<td>o permanent</td>
<td>o resonant</td>
<td>o radial</td>
</tr>
<tr>
<td>Dir. 3I0&gt; stage with sinφ measurement</td>
<td>o permanent</td>
<td>o isolated</td>
<td>o radial</td>
</tr>
<tr>
<td>Directional stage with phasor measurement of a harmonic</td>
<td>o permanent</td>
<td>o resonant</td>
<td>o radial</td>
</tr>
<tr>
<td>(will be considered in a later document version)</td>
<td>o isolated</td>
<td></td>
<td>o meshed</td>
</tr>
<tr>
<td>Directional transient ground-fault stage</td>
<td>o Permanent</td>
<td>o resonant</td>
<td>o radial</td>
</tr>
<tr>
<td></td>
<td>o Intermittent</td>
<td>o isolated</td>
<td>o meshed / ring</td>
</tr>
<tr>
<td></td>
<td>o transient</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Directional intermittent ground-fault protection 1)</td>
<td>o Intermittent</td>
<td>o resonant</td>
<td>o radial</td>
</tr>
<tr>
<td></td>
<td>o transient</td>
<td>o isolated</td>
<td>o meshed / ring</td>
</tr>
</tbody>
</table>

Table 1: function overview

1) The function Directional intermittent ground-fault protection has been innovated with version V7.3 in 07/2016 (e.g., sampling frequency change from 1 to 8 kHz; improved direction determination, ...).

The functions according to table 1 are the standard functions for this application. Further directional functions are available, which are used by specific customers due to their application history / philosophy.
2.1 General function selection considerations and recommendations

The following figure provides a tree-structure view on the recommended functions, depending on Ground fault type, Grounding type and Network structure.

Referring to Table 1 and Figure 1 the following conclusions / recommendations can be made:

**Permanent ground faults**
For the directional detection of a permanent ground fault we recommend applying a function with **stationary** directional measurement if this is possible with regards to grounding type and network structure. Stationary directional measurement provides the best reliability if the signals allow a clear direction determination. Stationary directional measurement is provided by the function **Directional 3I0> stage with cosφ measurement**. The function **directional transient ground-fault stage** provides no stationary directional measurement. The direction determination is only made during the ground fault inception.

- in case of **resonant grounded radial networks** we recommend applying **directional 3I0> stage with cosφ measurement**. An exception is the condition that the active ground fault current is very low due to marginal losses of the arc-suppression coil (Peterson coil). If the active ground fault current is too small to allow a reliable directional result, we recommend applying the **directional transient ground-fault stage**.

- in case of **resonant grounded and meshed networks** operational circulating ground currents are common which normally allow no reliable directional result via the active ground fault current. Therefore, we recommend applying **Directional transient ground-fault stage**.

- in case of **isolated networks** the reactive ground fault current generally allows a reliable directional result, independent of operational circulating ground currents. Therefore, we recommend applying the function **Directional 3I0> stage with sinφ measurement**.


**Intermittent ground faults**
For intermittent ground fault detection we recommend applying the function *Directional intermittent ground fault protection*, in parallel to the function selected for the permanent ground fault detection.

**Transient ground faults**
The *Directional transient ground-fault stage* must be applied. The application of this function is without alternative if transient ground faults shall be detected.
2.2 Location of the functions in the DIGSI library

The above listed functions are available in the DIGSI global library for defined devices types and defined function group types:

<table>
<thead>
<tr>
<th>Directional ground fault function (block) type</th>
<th>Function block name in DIGSI</th>
<th>Available in DIGSI under:</th>
<th>Available in function groups (most common FG) in DIGSI:</th>
</tr>
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<tr>
<td>Directional 3I0&gt; stage with cosφ or sinφ measurement</td>
<td>$3I0&gt;\cos/sin\phi$</td>
<td>- Gnd ft.prot. for resonant-gnd.Isol.</td>
<td>FG Voltage/current 3ph</td>
</tr>
<tr>
<td></td>
<td></td>
<td>- 51NS Sens. GFF</td>
<td>FG Line</td>
</tr>
<tr>
<td></td>
<td></td>
<td>- 67NS Dir.sens GFF</td>
<td>Line</td>
</tr>
<tr>
<td></td>
<td></td>
<td>- 67NS Dir.sens GFF</td>
<td>Line Line Line</td>
</tr>
<tr>
<td>Directional stage with phasor measurement of a harmonic</td>
<td>$V0&gt;\text{dir}.harm.$</td>
<td>- Gnd ft.prot. for resonant-gnd.Isol.</td>
<td>FG Voltage/current 3ph</td>
</tr>
<tr>
<td></td>
<td></td>
<td>- 51NS Sens. GFF</td>
<td>FG Line</td>
</tr>
<tr>
<td></td>
<td></td>
<td>- 67NS Dir.sens GFF</td>
<td>Line</td>
</tr>
<tr>
<td></td>
<td></td>
<td>- 67NS Dir.sens GFF</td>
<td>Line</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>…</td>
</tr>
<tr>
<td>Directional transient ground-fault stage</td>
<td>$\text{Trans.Gnd.ft}$</td>
<td>- Gnd ft.prot. for resonant-gnd.Isol.</td>
<td>FG Voltage/current 3ph</td>
</tr>
<tr>
<td></td>
<td></td>
<td>- 51NS Sens. GFF</td>
<td>FG Line</td>
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<td>- 67NS Dir.sens GFF</td>
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<td>- 67NS Dir.sens GFF</td>
<td>Line</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>…</td>
</tr>
<tr>
<td>Directional intermittent ground-fault protection</td>
<td>$\text{Dir.interm.gnd.ft}$</td>
<td>- Current protection</td>
<td>FG Voltage/current 3ph</td>
</tr>
<tr>
<td></td>
<td></td>
<td>- $\text{Dir.intermittent ground-fault prot.}$</td>
<td>FG Line</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>Line</td>
</tr>
<tr>
<td></td>
<td></td>
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<td>Line</td>
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<td>…</td>
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</table>
3 General configuration notes

3.1 Fault recording

With SIPROTEC 5 the oscillography recording capacity was extremely extended compared to SIPROTEC 4. Limited recording capacity is no issue for SIPROTEC 5.

Recommendation: SIEMENS generally recommends recording ground faults. This is essential for later ground fault analysis.

Further recommendations about recording function specific signals are given in the application description for the respective functions.

Configuration notes

1. Ground fault stages (function blocks)

For each protection / detection stage you can select if the fault recording shall be stated automatically, by keeping the following default setting:

| Operate & flt. rec. blocked | no |

With this setting also general pickup and tripping takes place. If this is not desired the setting can be changed to yes and fault recording can be started manually.

2. Fault recorder

The following figure shows the fault recorder setting list. The fault recording is started automatically with pickup. This requires that the parameter Operate & flt. rec. blocked of each stage or function is set to no (refer to above). If the parameter is set to yes the fault recording must be started manually.

The only change compared to the default is marked in red. Especially if one of the functions Directional transient ground-fault stage or Directional intermittent ground-fault protection is applied, it is essential setting the sampling frequency to 8 kHz. In case that none of these functions is applied the sampling frequency can remain on the default of 2 kHz.

Figure 2  Setting list
3.2 Fault logging

Setting and routing recommendations to avoid signals floods in a log are given in the individual function descriptions, in the “Further notes” chapter.

3.3 No tripping on ground faults

It could be required to keep the power system in operation during ground faults. Consequently, the ground fault protection functions shall only detect the ground fault but shall not trip.

**Recommendation:**

To avoid tripping, we do not recommend setting **Operate & flt.rec. blocked** to yes, because by this the automatic fault recording is disabled as well.

To avoid tripping, we recommend using the **Circuit-breaker interaction** matrix, by taking the respective functions and stages out of the trip-interface, as shown in the following figure for the 3I0>cos/sin stage. By this the protection stage operates but this signal is not forwarded to the tripping logic.

![Circuit-breaker interaction matrix](image)
4 Permanent ground fault detection

According to chapter 2.1 the function selection tree for a permanent ground fault is as following.

The following sub chapters are following the further selection according "grounding type" and "network structure".
4.1 Resonant-grounded, radial network

4.1.1 Function “Dir. 3I0>stage with Cosφ measurement”

Remark: For simplification this function (stage) is named as Cosφ in the following.

4.1.1.1 Setting notes

The following figure shows the stage settings. In the following setting notes and recommendations are given. The standard function control is not explained here. Further information can be taken from the device manual.

Figure 5 Setting list (in default state)

**Blk.by interm.gnd.flt.** (new with V8.01) special attention should be given

During intermittent ground faults, stages designed for detecting permanent ground faults (based on continuous RMS measurement, like the Cosφ stage) tend to generate a flood of signals and probably even temporary wrong directional information. This can be avoided by blocking these stages in case of an intermittent ground fault. If intermittent ground faults are probable in your network, Siemens strongly recommends enabling the blocking.

**Recommendation:** We propose to set Yes.

Additionally, the function block Blk.interm.GF need to be configured. Please refer to chapter 5.3.

**Blk.w. inrush curr. detec.**

You specify whether the operate is blocked during detection of an inrush current. Siemens recommends disabling the blocking. The fundamental component of the zero-sequence voltage is a reliable criterion for the ground fault detection and remains almost unaffected by switching-on procedures.

**Recommendation:** We propose disabling the blocking, set to No.

**Blk.after fault extinction**
Pickup can be blocked after detection of the fault extinction. With this, pickups are avoided due to the decay process in the zero-sequence system after the fault extinction.

**Recommendation**: We propose to set **Yes**.

**Directional mode**

The parameter **Directional mode** defines whether the pickup of the stage occurs in forward or backward direction. Usually, the stage should operate in case of forward ground faults, which requires to set **forward**.

**Dir. Measuring method, \( \phi \) Correction**

These parameters are used to define the direction characteristic of the stage. The direction characteristic depends on the neutral-point treatment of the system, which is in this consideration "arc-suppression coil (resonant) grounded".

The settings must be set to:

\[
\text{Dir. Measuring method} = \cos \phi
\]

\[
\phi \text{ Correction} = 0^\circ
\]

**Min. polar.3I_0> for dir.det.** [special attention should be given]

For \( \cos \phi \) measuring method with \( 0^\circ \) \( \phi \) correction the polarizing 3I_0> for the direction determination is the active (ohmic) component of the total 3I_0. Consequently, this setting is made with relation to the active (ohmic) component of the total 3I_0.

In the following we are providing two setting recommendations:

1. **Rule of thumb approach**: this approach is simple and gives good detection results if no detection up to a defined ground fault resistance is required
2. **Approach to detect ground faults till a defined ground-fault resistance**: this approach should be followed if ground faults must be detected up to a defined ground-fault resistance.

**Recommendation A: rule of thumb approach:**

The threshold is set in a range between 25% to 50% of the active zero sequence current \( 3I_{0 active} \). \( 3I_{0 active} \) can easily be determined from the known \( I_{CE} \) and the known network damping \( d \) (for further information about the formula and a setting example, please refer to chapter 7.2.17.2):

\[
3I_{0 active} = d \cdot I_{CE}
\]

\[
\text{Min. polar.3I_0> for dir.det.} = 0.25 \ldots 0.5 \cdot 3I_{0 active}, \text{ e.g. } 0.3 \cdot 3I_{0 active}
\]

**Recommendation B: approach to detect ground faults till a defined maximum ground fault resistance**

The threshold value is determined according to the approach to detect ground faults till a defined maximum ground fault resistance, e.g. \( 3 \) k\( \Omega \). The respective description, including a specific network example, is given in chapter 7.2.2.

**Note**: this setting is not feeder specific. The same setting applies to all feeders.

**\( \alpha_1 \) reduction dir. area, \( \alpha_2 \) reduction dir. area**

With the \( \alpha_1 \) reduction dir. area and \( \alpha_2 \) reduction dir. area parameters, you specify the angle for the limitation of the direction range. In feeders with a very large reactive current, it can be practical to set a larger angle than 2° to avoid a
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false pickup based on transformer and algorithm tolerances. You should only do this if you are aware of problems with the default setting of 2°.

**Recommendation:** We propose to keep the default of 2°.

**Threshold Value for 3I₀**

This setting relates to the total 3I₀.

In the following we are providing two setting recommendations:

1. **Rule of thumb approach:** this approach is simple and gives good detection results if no detection up to a defined ground fault resistance is required
2. **Approach to detect ground faults till a defined ground-fault resistance:** this approach should be followed if ground faults must be detected up to a defined ground-fault resistance.

**Recommendation A: rule of thumb approach:**

Set this parameter to the same value as setting Min. polar.3I₀ for dir.det. (refer to above). The total 3I₀ is always higher than the active 3I₀. Setting the same value ensures that the stage will always pickup if the active 3I₀ is greater the setting Min. polar.3I₀ for dir.det.

\[
3I₀ > \text{threshold value} = \text{Min. polar.3I₀ for dir.det.}
\]

**Recommendation B: approach to detect ground faults till a defined maximum ground fault resistance**

This setting is made with relation to the total 3I₀ of the specific feeder and with relation to a defined maximum ground-fault resistance, e.g. 3 kΩ. The respective description, including a specific network example, is given in chapter 7.2.2.

**Threshold Value for V₀**

The \( V₀ \) threshold setting is derived for the network. The derived setting is identically for all feeders.

In the following we are providing two setting recommendations:

1. **Rule of thumb approach:** this approach is simple and gives good detection results if no detection up to a defined ground fault resistance is required
2. **Approach to detect ground faults till a defined ground-fault resistance:** this approach should be followed if ground faults must be detected up to a defined ground-fault resistance.

**Recommendation A: rule of thumb approach:**

The threshold is set to a typical percentage value of the full displacement voltage (for further information please refer to the description / example given in chapter 7.1), e.g. 40%:

\[
V₀ > \text{threshold value} = 0.4 \cdot 57.7 \, V = 23 \, V
\]

**Recommendation B: approach to detect ground faults till a defined maximum ground fault resistance**

This setting is made with relation to a defined maximum ground-fault resistance, e.g. 3 kΩ. The respective description, including a specific network example, is given in chapter 7.1.1.
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**Dir. determination delay** special attention should be given

The start of the ground fault normally shows a transient behavior. This can lead to an incorrect direction decision. The direction determination can be delayed from the occurrence of the zero-sequence voltage with the Dir. determination delay parameter to achieve steady-state measurands.

**Recommendations:**
1) **without considering intermittent ground fault** (if no intermittent ground fault occur): 50 ms usually serves to pass the transient process.
   
   Dir. determination delay = 50 ms

2) **with considering intermittent ground fault** (intermittent ground faults can occur): If this time is set to a value which allows to classify an intermittent ground fault as “intermittent” and additionally, the intermittent ground fault blocking is configured, annunciation (signal floods and wrong directional results) by e.g. the Cosφ stage can be avoided. Intermittent cable faults should be classified as such within 200 ms (if the setting recommendations for the Intermittent ground-fault blocking stage are applied, refer to chapter 5.3.15.1.1). For overhead lines intermittent ground faults are rare and classification usually last longer. We recommend focusing on intermittent cable faults and setting a delay of 200 ms.
   
   Dir. determination delay = 200 ms

**Note:** this delay time also delays the start of the operate delay timer. If you want to achieve a defined operate (trip) time with reference to the ground fault entry (V0 occurrence) you must reduce the operate delay by this time.

**Example:** Tripping shall occur 1 s after ground fault entry (V0 occurrence):

   Dir. determination delay = 200 ms
   Operate delay = 0.80 s

**Operate delay**

Must be set according to individual application requirements.

---

**4.1.1.2 Routing notes**

We recommend the following routing for operational log (column O), fault log (column F) and Recorder. This routing allows reliable ground fault clarification.
Figure 6  Signal list with recommended routing

Remark: since all relevant information of the Pickup signal are routed additional routing of the Ground fault signals is not required.

4.1.1.3 Further notes

Avoiding floods of logs and recordings in case of intermittent ground faults

Option A (recommended):

The stage can be automatically blocked during intermittent ground faults (by configuration, refer to the setting notes above). By this blocking floods of logs and recordings are effectively avoided if the Intermittent ground-fault blocking stage is well configured. Especially the parameter Reset time must not be set too short. For the description of this blocking stage and its setting recommendations please refer to chapter 5.3.

Option B (alternative):

If the blocking-feature cannot be applied for any reason, the following configuration can be applied to avoid log and recording floods:

1. Set the Fault recorder to user-defined recording. By this the fault recording and fault logging is no longer controlled via the pickup state of the protection function but via the signals routed into the recorder trigger column (refer to further below).
2. Setting the recording to **user-defined** offers the new recorder column **Trigger**. The recording duration is now determined from the logical OR operation of all active signals routed into the trigger column. Controlling fault recording (and fault logging) for ground-faults requires to only route the **Ground fault.general** SPS signal of the function block **General** into the trigger column.

**Note 1:** Do not mix this up with the **Ground fault.general** SPS signal of the **Transient ground-fault function**. It is essential to route the signal out of the function block **General**.

**Note 2:** If also short-circuit protection is applied in the device you must also route the **Pickup** group indications of each applied protection function group into the Trigger column.

3. For Parameter **Dropout delay** in the function block **General** the default value of 1 s should be kept. This value must not be set lower. With this setting the **Ground fault.general** signal of the function block **General** is hold during an intermittent fault till the next re-strike. In this way this signal remains active over the intermittent fault and the recording is not closed, i.e. no new recording is started. Consequently, a flood of recordings and longs is avoided.

### Avoiding floods of signals in case of intermittent ground faults

**Option A** (recommended):

The \( \cos \phi \) stage can be automatically blocked during intermittent ground faults (by configuration, refer to the setting notes above). By this blocking **signal floods** are effectively avoided.

**Option B** (alternative):
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If the blocking feature cannot be applied for any reason, we recommend a different signal routing as the one proposed in chapter 4.1.1.2. The signal **ground fault** (including the directional information) is stabilized against signal floods, as indicated in the following diagram. For this signal only a defined number of signal changes are recorded for one ground fault. After that logging for this signal is stopped.

![Figure 10](image-url) Excerpt from stage logic

The following diagram shows the recommended signal routing if the automatic blocking feature is not applied.

![Figure 11](image-url) Recommended routing to avoid signal flooding during intermittent ground faults.

**Remark:** take the routing for the **pickup** signal away and use instead the stabilized **ground fault** signal.
4.1.2 Function “Dir. Transient ground fault stage”

4.1.2.1 Setting notes

The following figure shows the stage settings. In the following setting notes and recommendations are given. The standard function control is not explained here. Further information can be taken from the device manual.

![Setting list](image)

**Blk. after fault extinction**

If the **Blk. after fault extinction** parameter is set to yes, the tripping delay is reset after the detection of the fault extinction. During intermittent faults fault extinction will be detected if the time between fault extinction and next restrike is long enough. If the function shall trip on intermittent faults this setting must be set to no.

Since in this application scenario (this chapter) the stage is applied for permanent ground faults this setting can be set yes.

**Operate functionality**

If the stage is used only to indicate the ground fault direction, this optional trip logic is not required and can remain disabled. If the stage is used to trip a permanent or intermittent ground fault the optional trip logic must be switched on.

**Setting is application dependent:** must be set to yes if the stage shall support tripping

**Directional mode**

The parameter **Directional mode** defines whether the pickup of the stage occurs in forward or backward direction. Usually, the stage should operate in case of forward ground faults, which requires to set forward.

**V0> threshold value**

The V0 threshold setting is derived for the network. The derived setting is identically for all feeders.
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In the following we are providing two setting recommendations:

1. **Rule of thumb approach**: this approach is simple and gives good detection results if no detection up to a defined ground fault resistance is required
2. **Approach to detect ground faults till a defined ground-fault resistance**: this approach should be followed if ground faults must be detected up to a defined ground-fault resistance.

**Recommendation A: rule of thumb approach:**

The threshold is set to a typical percentage value of the full displacement voltage (for further information please refer to the description / example given in chapter 7.1), e.g. 40%:

\[
V_0 > \text{threshold value} = 0.4 \cdot 57.7 \, \text{V} = 23 \, \text{V}
\]

**Recommendation B: approach to detect ground faults till a defined maximum ground fault resistance**

This setting is made with relation to a defined maximum ground-fault resistance, e.g. 3 kΩ. The respective description, including a specific network example, is given in chapter 7.1

**Maximum operational V0**

With the parameter Maximum operational V0, you define the maximum operational zero-sequence voltage \(V_{0\text{op,max}}\). The setting is needed for special reset conditions.

The secondary operational zero-sequence voltages can be obtained by reading the residual voltage \(V_{\text{Nsec}}\) or the zero-sequence voltage \(V_{0\text{sec}}\) under the symmetrical components from the device or via DIGSI.

In case you read the secondary residual voltage \(V_{\text{Nsec}}\), you convert it to \(V_{0\text{sec}}\) with the *Matching ratio Vph / VN* parameter. Its setting is usually \(\sqrt{3}\).

**Recommendation:**

- If the maximum operational zero-sequence voltage is known, set the threshold to 1.2 \(V_{0\text{op,max}}\)
- If the maximum operational zero-sequence voltage is unknown and cannot be determined for any reason, please keep the default of 3V

**Example:**

- Maximum operational secondary residual voltage reading: \(V_{\text{Nsec}} = 5.0 \, \text{V}\)
- Matching ratio Vph / VN = \(\sqrt{3}\)
- \(V_{0\text{sec}} = 5.000 \, \text{V} \cdot \sqrt{3} / 3 = 2.887 \, \text{V}\)
- **Maximum operational V0** = \(2.887 \, \text{V} \cdot 1.2 = 3.464 \, \text{V}\)

**3I0> threshold for pickup**

In ring or meshed systems, you can use this parameter to reduce the number of ground-fault reporting devices. The parameter needs to be set according to the user experience on the specific network. For radial systems, normally you can keep the default value of 0 A which sets this parameter to inactive.

**Recommendation**: set this functionality inactive by keeping the default value of **0 A**

**3I0> threshold for operate**

The setting is significant only for optional trip logic for switching off permanent ground faults. Select the setting such that the static ground-fault current exceeds the threshold value. You can disable this criterion by setting the value to 0 A.
If the function shall be applied to trip intermittent ground faults (which is the case for this specific chapter description) the threshold could be undershoot during the phase between fault extinction and next restrike, causing the operate delay timer to reset. To avoid this risk the threshold should be set to 0 A.

**Recommendation:** set this criterion inactive by setting the threshold to 0 A

**Operate delay**

Must be set according to individual application requirements.

**Dropout delay**

Parameter **Dropout delay** allows you to use the stage effectively for tripping intermittent ground faults. For respective setting recommendations please refer to chapter 5.2.1.

Since in this application scenario (this chapter) the stage is applied for permanent ground faults this setting can be set 0 s.

**Recommendation:** set this functionality inactive by keeping the default value of 0.00 s

### 4.1.2.1 Routing notes

We recommend the following routing for operational log (column O), fault log (column F) and Recorder. This routing allows reliable ground-fault clarification.

**Transient Ground Fault Function:**

<table>
<thead>
<tr>
<th>Signal list with recommended routing for the Transient Ground Fault Function</th>
</tr>
</thead>
</table>

Function block **General:**
Figure 14  Signal list with recommended routing for the FB General

We recommend routing the signal **Pos. measuring window** into the fault recorder. This signal is essential for later ground-fault clarifications.

### 4.1.2.2 Further notes

**Avoiding floods of logs and recordings in case of intermittent ground faults**

The stage is fully immune against generating such floods during intermittent ground faults. No measures need to be taken.

**Avoiding floods of signals in case of intermittent ground faults**

The stage is fully immune against generating such floods during intermittent ground faults. No measures need to be taken.
4.2 Resonant-grounded, meshed / ring network
[To be added at a later state]

4.3 Isolated network
For the detection of permanent ground faults in isolated networks the Dir. 3I0>stage with \( \sin \phi \) measurement is the most applied standard function.

4.3.1 Function “Dir. 3I0>stage with \( \sin \phi \) measurement”
Remark: For simplification this function (stage) is named as \( \sin \phi \) in the following.

4.3.1.1 Setting notes
The following figure shows the stage settings. In the following setting notes and recommendations are given. The standard function control is not explained here. Further information can be taken from the device manual.

![Setting list](image)

**Blk.by interm.gnd.flt. (new with V8.01) special attention should be given**

During intermittent ground faults, stages designed for detecting permanent ground faults (based on continuous RMS measurement, like the \( \sin \phi \) stage) tend to generate a flood of signals and probably even temporary wrong directional information. This can be avoided by blocking these stages in case of an intermittent ground fault. If intermittent ground faults are probable in your network, Siemens strongly recommends enabling the blocking.

**Recommendation:** We propose to set Yes.

Additionally, the function block **Blk.interm.GF** need to be configured. Please refer to chapter 5.3.
You specify whether the operate is blocked during detection of an inrush current. Siemens recommends disabling the blocking. The fundamental component of the zero-sequence voltage is a reliable criterion for the ground fault detection and remains almost unaffected by switching-on procedures.

**Recommendation:** We propose disabling the blocking, set to No.

**Blk.after fault extinction**

Pickup can be blocked after detection of the fault extinction. With this, pickups are avoided due to the decay process in the zero-sequence system after the fault extinction.

**Recommendation:** We propose to set Yes.

**Directional mode**

The parameter **Directional mode** defines whether the pickup of the stage occurs in forward or backward direction. Usually, the stage should operate in case of forward ground faults, which requires to set **forward**.

**Dir. Measuring method, φ Correction**

These parameters are used to define the direction characteristic of the stage. The direction characteristic depends on the neutral-point treatment of the system, which is in this consideration "isolated".

The settings must be set to:

- **Dir. Measuring method** = Sin φ
- **φ Correction** = 0°

**Min. polar.3I0> for dir.det.** special attention should be given

For Sin φ measuring method with 0° φ correction the polarizing 3I0> for the direction determination is the capacitive component of the total 3I0. However, in an isolated network the active (ohmic) component of the total 3I0 is neglectable. Consequently, the capacitive 3I0 and the total 3I0 are the same.

In the following we are providing two setting recommendations:

1. **Rule of thumb approach:** this approach is simple and gives good detection results if no detection up to a defined ground fault resistance is required
2. **Approach to detect ground faults till a defined ground-fault resistance:** this approach should be followed if ground faults must be detected up to a defined ground-fault resistance.

**Recommendation A: rule of thumb approach:**

The threshold is set in to 30% of the capacitive zero-sequence current 3I0\textsubscript{cap,fd} flowing in the faulty feeder. 3I0\textsubscript{cap,fd} can easily be determined from the known ICE for the network and the known ICE of the individual feeder:

\[
3I0\textsubscript{cap,fd} = I_{CE} - I_{CE,feeder}
\]

**Min. polar.3I0> for dir.det.** = 0.3 \times (I_{CE} - I_{CE,feeder})

**Example:**

- I_{CE} = 200 A
- I_{CE,feeder} = 40 A

Min. polar.3I0> for dir.det. = 0.3\times(200 A - 40 A) = 48 A (primary)
Directional ground fault detection in resonant-grounded or isolated networks

**Recommendation B: approach to detect ground faults till a defined maximum ground fault resistance**

The threshold value is determined according to the approach to detect ground faults till a defined maximum ground fault resistance, e.g. 300 Ω. The respective description, including a specific network example, is given in chapter 7.2.3.

**Note:** this setting is feeder specific. The setting needs to be determined for each feeder individually.

**α1 reduction dir. area, α2 reduction dir. area**

With the α1 reduction dir. area and α2 reduction dir. area parameters, you specify the angle for the limitation of the direction range. In feeders with a very large reactive current, it can be practical to set a larger angle than 2° to avoid a false pickup based on transformer and algorithm tolerances. You should only do this if you are aware of problems with the default setting of 2°.

**Recommendation:** We propose to keep the default of 2°.

**3I0> threshold value** __special attention should be given__

This setting relates to the total 3I0. As the capacitive 3I0 and the total 3I0 are the same in an isolated network this setting is set to the same value as determined for parameter Min. polar.3I0> for dir.det., refer to above.

**V0> threshold value** __special attention should be given__

The V0 threshold setting is derived for the network. The derived setting is identically for all feeders.

In the following we are providing two setting recommendations:

3. **Rule of thumb approach:** this approach is simple and gives good detection results if no detection up to a defined ground fault resistance is required

4. **Approach to detect ground faults till a defined ground-fault resistance:** this approach should be followed if ground faults must be detected up to a defined ground-fault resistance.

**Recommendation A: rule of thumb approach:**

The threshold is set to a typical percentage value of the full displacement voltage (for further information please refer to the description / example given in chapter 7.1). For isolated networks we recommend a rather low typical percentage (30 %) as the zero-sequence voltage drops rather fast for increasing fault resistance.

\[
V0> \text{threshold value} = 0.3 \cdot 57.7 \text{ V} = 17 \text{ V}
\]

**Recommendation B: approach to detect ground faults till a defined maximum ground fault resistance**

This setting is made with relation to a defined maximum ground-fault resistance, e.g. 300 Ω. The respective description, including a specific example, is given in chapter 7.1.2.

**Dir. determination delay** __special attention should be given__

The start of the ground fault normally shows a transient behavior. This can lead to an incorrect direction decision. The direction determination can be delayed from the occurrence of the zero-sequence voltage with the Dir. determination delay parameter to achieve steady-state measurands.
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**Recommendations:**

1) **without considering intermittent ground fault** (if no intermittent ground fault occur): 50 ms usually serves to pass the transient process.

   \[ \text{Dir. determination delay} = 50 \text{ ms} \]

2) **with considering intermittent ground fault** (intermittent ground faults can occur): If this time is set to a value which allows to classify an intermittent ground fault as “intermittent” and additionally, the intermittent ground fault blocking is configured, annunciation (signal floods and wrong directional results) by e.g. the Cosφ stage can be avoided. Intermittent cable faults should be classified as such within 200 ms (if the setting recommendations for the **Intermittent ground-fault blocking** stage are applied, refer to chapter 5.3.1). For overhead lines intermittent ground faults are rare and classification usually last longer. We recommend focusing on intermittent cable faults and setting a delay of 200 ms.

   \[ \text{Dir. determination delay} = 200 \text{ ms} \]

**Note:** this delay time also delays the start of the operate delay timer. If you want to achieve a defined operate (trip) time with reference to the ground fault entry (V0 occurrence) you must reduce the operate delay by this time.

**Example:** Tripping shall occur 1 s after ground fault entry (V0 occurrence):

   \[ \text{Dir. determination delay} = 200 \text{ ms} \]
   \[ \text{Operate delay} = 0.80 \text{ s} \]

**Operate delay**

Must be set according to individual application requirements.

**4.3.1.2 Routing notes**

We recommend the following routing for operational log (column O), fault log (column F) and Recorder. This routing allows reliable ground fault clarification.
4.3.1.3 Further notes

For

- Avoiding floods of logs and recordings in case of intermittent ground faults
- Avoiding floods of signals in case of intermittent ground faults

Refer to chapter 4.1.1.3.

4.3.2 Function “Dir. Transient ground fault stage”

[To be added at a later state]
5 Intermittent ground fault detection

According to chapter 2.1 the function selection tree for an intermittent ground fault is as following.

The following two functions are available for the directional detection of intermittent ground faults:

- Directional intermittent ground-fault protection
- Directional transient ground-fault stage

Both functions can be applied independently of grounding type and network structure.

The main technical differences between these two functions are as following:

| Basic ground-fault criterion magnitude (function trigger) | 3I0 | V0 |
| Direction determination | With each new detected ground current peak (restrike) | Only at the ground fault entry (via charging transient). During the ongoing intermittent fault (restriking) no further direction determination is made. |
| Stationary measurement | Directional determination is “quasi stationary” | Direction is evaluated only with fault start and then kept. Direction changes during the intermittent faults are not detected. |
| Intermittent fault-type annunciation | Yes | No (no differentiation between permanent and intermittent fault type) |
| Detection of a permanent (steady state) fault | No (with pulse counting mode) Yes (with p.u. time integration) | Yes |
| Sensitivity | Medium | High |
Function selection considerations / recommendations

In case that no preference for one or the other function is given by the customer (due to philosophy / experience), Siemens recommends applying the Dir. Intermittent ground fault protection function. The reason for this is the "quasi stationary" directional measurement which provides a maximized reliability and the fact that the function can characterize the fault as "intermittent".
5.1 Function “Dir. Intermittent ground fault protection”

5.1.1 Setting notes

The following figure shows the function settings. In the following setting notes and recommendations are given. The standard function control is not explained here. Further information can be taken from the device manual.

Directional mode

Here one defines if the function operates in forward or in reverse direction. Usually, the stage should operate in case of forward ground faults, which requires to set forward.

Pickup mode

- With 3I0: pickup takes place if the absolute value of 3I0 exceeds the pickup threshold. The determined direction is not considered in the pickup condition.
- With direction: pickup takes place if a) the absolute value of 3I0 exceeds the pickup threshold and b) the determined direction is equal to the set direction.

Recommendation: We propose setting With 3I0. In this way all intermittent faults are logged and recorded which serves for a better fault analysis.

Operating mode, No. of pulses for operate special attention should be given

Two operating modes for the operating (tripping) mode are available. They are explained by the following figures:

- Counter: Counting directional 3I0 pulses

For each re-strike (3I0 pulse) the direction is determined. The directional pulses are counted. For the example in Figure 19 these are four pulses (red numbers 1..4) and in Figure 20 eight pulses (red numbers 1..8), e.g. with the direction "forward".
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The following figure shows the counters. Assuming a detected forward direction for each pulse the pulse-forward-counter has the value 4 for the first example and 8 for the second example. And the two other counters have the value 0.

If the counter for the set direction reaches the setting value of parameter No. of pulses for operate the function trips.

Recommendation: We propose the operating mode Counter due to its simple principle. However, it can be noted that the pulse counter is much faster increased for fast and periodically re-striking ground fault (refer to Figure 20, characteristic 2) than for a ground fault characteristic acc. Figure 19. If no specific tripping time requirements are given the following is a practical value for tripping:

No. of pulses for operate = 5

With this setting the tripping time for the two different characteristics is approx.: 1.3 s .. 1.4 s for characteristic 1 and 0.25 s for characteristic 2

If a minimum trip delay time is required (e.g. 2 s), we recommend implementing a CFC to serve this requirement. A respective CFC proposal is given in chapter 7.4.

With firmware version V8.3 this minimum operate delay time is introduced as a new function parameter and can be set directly in the function. No CFC will be required.
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- **Integrator and counter:** Counting directional 3I0 pulses and integration of the pick-up time of the 3I0 RMS fault current stage, for time grading coordination

Additionally, to the directional pulse counting, the time periods in which the 3I0 is above the set threshold (blue line in Figure 19, periods t1, t2, t3) are integrated. If the integration value exceeds a set threshold this additional tripping criterion is fulfilled. In this way a time grading can be achieved. We consider this as a rare application. Therefore, we do not further explain this mode and the further involved setting.

**Threshold**

special attention should be given

3I0 is calculated as true-RMS quantity to also measure non-fundamental components (the current peak). The threshold must be set in a way that the 3I0 peaks (pulses) significantly exceeds the threshold.

This setting value relates to the total 3I0.

In the following we are providing two setting recommendations:

1. **Rule of thumb approach:** this approach is simple and gives good detection results if no detection up to a defined ground fault resistance is required
2. **Approach to detect ground faults till a defined ground-fault resistance:** this approach should be followed if ground faults must be detected up to a defined ground-fault resistance.

**Recommendation A: rule of thumb approach:**

Set this parameter to 50% of the active 3I0 component of the network and therefore independent from the individual feeder I_{CE}. By this the compensation type (over or under) and the compensation degree does not need to be considered as well. For further simplification the damping (active component) is considered as 3% of the network I_{CE}.

Threshold value = 0.5 \cdot 0.03 \cdot I_{CE,\text{network}}

**Recommendation B: approach to detect ground faults till a defined maximum ground fault resistance**

This setting is made with relation to the total 3I0 of the specific feeder and with relation to a defined maximum ground-fault resistance, e.g. 3 kΩ. The respective description, including a specific network example, is given in chapter 7.2.2.

**Note:** The 3I0 threshold derived according to chapter 7.2.2 relates to a permanent ground-fault. During an intermittent ground fault, the 3I0 fault current level will not fully reach the fault current level for a permanent ground fault. Therefore, please follow the additional recommendation given in chapter 0.

**Pickup extension time**

This parameter is only required in case of time grading coordination with old relays that have different pickup and dropout timing. This is a very specific condition that is not further considered.

**Recommendation:** keep the default value

**No. of pulses for interm. GF**

With this parameter you set the total number of pulse counts (sum of forward, reverse and non-dir. pulses) at which the ground fault is considered being intermittent.
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**Recommendation:** keep the default value of 3 pulses

**Note:** this setting value must be set smaller or equal to the setting value of **No. of pulses for operate**

**Reset time**

special attention should be given

The function is reset when it trips. Reset of the function mostly means that the pulse-counters are reset. If no trip occurs the function-reset is controlled by the reset timer. The reset timer is newly started (timer reset) with each new exceeding of the 3I0 threshold (with each new function pickup). If the timer expires the function resets.

Intermittent cable faults can show fast re-striking in the area of 1...2 network periods up to re-striking with intervals in the range of few seconds.

Depending on the pickup threshold setting and the intermittent fault characteristic (fast and periodically re-striking for a cable faults 3I0 does not drop below the dropout threshold during the intermittent fault. The reset timer is then **not** newly started (reset). Therefore, the reset timer must be set in a way that it does not expire before tripping.

**Recommendation:** a practical value to a) handle the condition that during the fault no dropout occurs and b) consider an intermittent fault as disappeared is e.g. **10 s**.
5.1.2 Routing notes

We recommend the following routing for operational log (column O), fault log (column F) and Recorder. This routing allows reliable ground fault clarification.

![Signal list with recommended routing](Figure 22)

5.1.3 Further notes

**Avoiding floods of logs and recordings in case of intermittent ground faults**

The function is specifically designed in a way that for one intermittent ground fault only one fault recording, and one fault log is created. However, this requires setting parameter Reset time in a correct way, as described under the setting notes. No further measures need to be taken.

**Avoiding floods of signals in case of intermittent ground faults**

With the signal routing according to chapter 5.1.2 the fault log will not be flooded during an intermittent ground fault. The signal Limited pickup (log) serves this by limiting the signal state change during an intermittent ground fault.
5.2 Function “Dir. Transient ground fault stage”

5.2.1 Setting notes

The following figure shows the stage settings. In the following setting notes and recommendations are given. The standard function control is not explained here. Further information can be taken from the device manual.

![Stage settings diagram]

**Blk. after fault extinction**

special attention should be given

If the **Blk. after fault extinction** parameter is set to **yes**, the tripping delay is reset after the detection of the fault extinction. During intermittent faults fault extinction will be detected if the time between fault extinction and next restrick is long enough. Since in this application scenario this stage shall be applied to trip on intermittent faults this setting must be set to **no**.

**Setting is application dependent:** must be set to **no** if the stage shall be applied for tripping intermittent faults

**Operate functionality**

If the stage is used only to indicate the ground fault direction, this optional trip logic is not required and can remain disabled. If the stage is used to trip a permanent or intermittent ground fault the optional trip logic must be switched on.

**Setting is application dependent:** must be set to **yes** if the stage shall support tripping

**Directional mode**

The parameter **Directional mode** defines whether the pickup of the stage occurs in forward or backward direction. Usually the stage should operate in case of forward ground faults, which requires to set **forward**.

**V0> threshold value**

special attention should be given

The V0 threshold setting is derived for the network. The derived setting is identically for all feeders.

In the following we are providing two setting recommendations:
3. **Rule of thumb approach**: this approach is simple and gives good detection results if no detection up to a defined ground fault resistance is required.

4. **Approach to detect ground faults till a defined ground-fault resistance**: this approach should be followed if ground faults must be detected up to a defined ground-fault resistance.

**Recommendation A: rule of thumb approach**:

The threshold is set to a typical percentage value of the full displacement voltage (for further information please refer to the description / example given in chapter 7.1). Since the displacement voltage for an intermittent fault is not reaching the same level as for a permanent fault a lower typical percentage value of 30% is recommended:

\[ V_0 > \text{threshold value} = 0.3 \cdot 57.7 \text{ V} = 17 \text{ V} \]

**Recommendation B: approach to detect ground faults till a defined maximum ground fault resistance**

This setting is made with relation to a defined maximum ground-fault resistance, e.g. 3 kΩ. The respective description, including a specific network example, is given in chapter 7.1.3

**Maximum operational V0 special attention should be given**

With the parameter Maximum operational V0, you define the maximum operational zero-sequence voltage \( V_{0,\text{op, max}} \). The setting is needed for special reset conditions.

The secondary operational zero-sequence voltages can be obtained by reading the residual voltage \( V_{N,\text{sec}} \) or the zero-sequence voltage \( V_{0,\text{sec}} \) under the symmetrical components from the device or via DIGSI.

In case you read the secondary residual voltage \( V_{N,\text{sec}} \), you convert it to \( V_{0,\text{sec}} \) with the Matching ratio \( V_{\text{ph}} / V_{N} \) parameter. Its setting is usually \( \sqrt{3} \).

**Recommendation**:

- If the maximum operational zero-sequence voltage is known, set the threshold to 1.2 \( V_{0,\text{op, max}} \)
- If the maximum operational zero-sequence voltage is unknown and cannot be determined for any reason, please keep the default of 3V

**Example**:

- Maximum operational secondary residual voltage reading: \( V_{N,\text{sec}} = 5.0 \text{ V} \)
- Matching ratio \( V_{\text{ph}} / V_{N} = \sqrt{3} \)
- \( V_{0,\text{sec}} = 5.000 \text{ V} \cdot \sqrt{3} / 3 = 2.887 \text{ V} \)
- **Maximum operational V0** = \( 2.887 \text{ V} \cdot 1.2 = 3.464 \text{ V} \)

**3I0> threshold for pickup**

In ring or meshed systems, you can use this parameter to reduce the number of ground-fault reporting devices. The parameter needs to be set according to the user experience on the specific network. For radial systems, normally you can keep the default value of 0 A which sets this parameter to inactive.

**Recommendation**: set this functionality inactive by keeping the default value of 0 A

**3I0> threshold for operate**

The setting is significant only for optional trip logic for switching off permanent ground faults. Select the setting such that the static ground-fault current exceeds the threshold value. You can disable this criterion by setting the value to 0 A.
If the function shall be applied to trip intermittent ground faults (which is the case for this specific chapter description) the threshold could be undershoot during the phase between fault extinction and next restrike, causing the operate delay timer to reset. To avoid this risk the threshold should be set to 0 A.

**Recommendation:** set this criterion inactive by setting the threshold to 0 A

**Operate delay**

Must be set according to individual application requirements.

**Dropout delay**

Parameter **Dropout delay** allows you to use the stage effectively for tripping intermittent ground faults. With the dropout delay, the pickup state after fault extinction is held until the next ignition (re-strike). Thus, the operate delay is not reset and can trip the fault. Set the time to a value within which the new ignition can still be assigned to the previous ignition. Typical values are in a range between several hundred milliseconds and a few seconds.

**General Recommendation:** The **Dropout delay** timer should not be set higher than 1/3 the operate delay. Otherwise, there is a risk that the stage trips on one single ground fault transient.

E.g. if the operate delay is 2 s, the dropout delay timer should be set < 0.66 s.

**Example 1:**

In the preceding figure an ordinary intermittent cable ground-fault is presented. Immediately after an ignition the extinction takes place, and the zero sequence signals are decaying. During the decaying phase the V0> pickup threshold is undershooting (as indicated in the figure). Without applying the dropout delay the **operate delay** timer would be reset and no tripping would take place.

The duration between the single ignitions varies in the range from approx. 270 ms to 390 ms. A set dropout delay of e.g. 500 ms would safely ensure that the V0> pickup threshold is exceeded again with the next ignition and that the operate delay timer continues to run. If the operate delay would be set to e.g. 2 s the stage would trip after 2 s.

For example 1: **dropout delay = 0.5 s**
It must be noted that tripping could then take place 2 s (= operate delay) after the first fault ignition with only 2 re-strikes (assumptions that a) V0> threshold value is set to a quite low value so that undershooting this value takes place ~200 ms after fault extinction, and b) the re-striking take place shortly before the dropout delay expires)

Example 2:

![Graph](image)

Example 2 is an intermittent ground fault with much more frequent re-striking (ignitions). Consequently, the decaying time between extinction and next ignition is too short to allow VN dropping below the V0> pickup threshold. If one could rely on this periodically frequent re-striking no dropout delay would be required. However, since such a characteristic is not fully reliable, we recommend to also set a dropout delay of e.g. 0.5 s, if the operate delay is set at least 3 times higher (> 1.5 s).

For example 2: dropout delay = 0.5 s

### 5.2.2 Routing notes

We recommend the following routing for operational log (column O), fault log (column F) and Recorder. This routing allows reliable ground-fault clarification.

#### Transient Ground Fault Function:

![Signal List](image)

**Figure 25** Signal list with recommended routing for the Transient Ground Fault Function

**Function block** General:
Directional ground fault detection in resonant-grounded or isolated networks

We recommend routing the signal **Pos. measuring window** into the fault recorder. This signal is essential for later ground-fault clarifications.

### 5.2.3 Further notes

**Avoiding floods of logs and recordings in case of intermittent ground faults**

The stage is fully immune against generating such floods during intermittent ground faults. No measures need to be taken.

**Avoiding floods of signals in case of intermittent ground faults**

The stage is fully immune against generating such floods during intermittent ground faults. No measures need to be taken.
5.3 Intermittent Ground Fault Blocking Stage (V8.01)

Most functions designed for the detection of permanent ground faults may show a disadvantageous behavior in case of intermittent ground faults. An example of these functions is the 3I0> stage with cos ϕ or sin ϕ measurement. In case of an intermittent ground fault, these functions may cause a flood of information due to continuously exceeding and dropping below thresholds. Also, short-term wrong directional results are possible due to the nature of the intermittent signals. To avoid this disadvantage, these functions should be blocked in case of intermittent grounds faults. The Intermittent ground-fault blocking stage detects and classifies a ground fault as intermittent and sends a blocking signal to the respective stages. The receiving stages – if configured accordingly – are then automatically blocked.

5.3.1 Setting notes

The following figure shows the function settings. In the following setting notes and recommendations are given.

![Setting list](image)

Figure 27 Setting list (in default state)

**Mode**

With the mode parameter the function block is switched on.

**Threshold**

With the parameter Threshold, you set the intermittent ground-fault pickup threshold. This setting must be coordinated with the applied protection stage for detecting a permanent ground fault, which shall be blocked for an intermittent fault, for example, the 3I0> stage with cos ϕ or sin ϕ measurement. The parameter Threshold must be set to the same value as the respective 3I0> threshold value of the protection stage.

In case of the 3I0> stage with cos ϕ or sin ϕ measurement, the value from the parameter (:12601:101) 3I0> threshold value must be applied for the parameter Threshold. It is not required to set a lower value than the respective 3I0> threshold value of the protection stage.

**Example**:
- Stage 3I0> stage with cos ϕ or sin ϕ measurement, parameter 3I0> threshold value = 105 mA (secondary)
- Stage Intermittent ground-fault blocking, parameter threshold = 105 mA (secondary)

**No.of pulses for intermittent.GF**

With the parameter No.of pulses for intermittent.GF, you set the total number of pulse counts at which the ground fault is classified as an intermittent fault. We consider three pulses as a good classification criterion.

**Recommendation**: We recommend keeping the default, which is 3.

The following figure shows a typical intermittent ground fault in a cable with high-frequent re-striking. The detected pulses and their counts are indicated. For this specific case the fault would be classified as “intermittent” with pulse indication “3”, approx. 170 ms after ground fault entry.
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The following figure shows an intermittent ground fault with lower frequent re-striking. For this specific case the fault would be classified as “intermittent” with pulse indication “3”, approx. 650 ms after ground fault entry.

Reset time

With the parameter Reset time, you define the minimum time between 2 adjacent ground faults. If the time is larger than the Reset time, the intermittent ground fault is considered as disappeared. This can mean that the ground fault has disappeared or that the intermittent ground fault has changed to a static ground fault. The function resets and a blocking is terminated. A typical value to consider an intermittent fault as gone is 5 s.

Recommendation: We recommend keeping the default, which is 5 s.

5.3.2 Routing notes

We recommend the following routing for operational log (column O), fault log (column F) and Recorder. This routing allows reliable ground fault clarification.

Figure 28  Typical intermittent cable ground-fault with high-frequent re-striking

Figure 29  Intermittent cable ground-fault with lower frequent re-striking

Figure 30  Signal list
6 Transient ground fault detection

According to chapter 2.1 the function selection tree for an intermittent ground fault is as following.

![Function selection tree for transient ground fault](image)

**Note:** the function application in this chapter assumes that the function shall be only applied to detect a transient ground fault. I.e. the function is **not** applied for tripping.

### 6.1 Function “Dir. Transient ground fault stage”

#### 6.1.1 Setting notes

The following figure shows the stage settings. In the following setting notes and recommendations are given. The **standard function control** is not explained here. Further information can be taken from the device manual.

![Setting list for Dir. Transient gnd. flt. stage](image)
Blk.after fault extinction

Since in this application scenario (this chapter) the stage is applied for transient ground fault detection, the default setting can be applied, which is yes.

Operate functionality

Since in this application scenario (this chapter) the stage is applied for transient ground fault detection, the default setting can be applied, which is no.

Directional mode

The parameter Directional mode defines whether the pickup of the stage occurs in forward or backward direction. Usually, the stage should operate in case of forward ground faults, which requires to set forward.

V0> threshold value special attention should be given

The V0 threshold setting is derived for the network. The derived setting is identically for all feeders.

In the following we are providing two setting recommendations:

5. Rule of thumb approach: this approach is simple and gives good detection results if no detection up to a defined ground fault resistance is required
6. Approach to detect ground faults till a defined ground-fault resistance: this approach should be followed if ground faults must be detected up to a defined ground-fault resistance.

Recommendation A: rule of thumb approach:

The threshold is set to a typical percentage value of the full displacement voltage (for further information please refer to the description / example given in chapter 7.1.2). Since the displacement voltage for a transient fault is not reaching the same level as for a permanent fault a lower typical percentage value of 30% is recommended:

\[ V_{0> \text{threshold value}} = 0.3 \times 57.7 \text{ V} = 17 \text{ V} \]

Recommendation B: approach to detect ground faults till a defined maximum ground fault resistance

This setting is made with relation to a defined maximum ground-fault resistance, e.g. 3 kΩ. The respective description, including a specific network example, is given in chapter 7.1.3.

Maximum operational V0 special attention should be given

With the parameter Maximum operational V0, you define the maximum operational zero-sequence voltage V0_{op,max}. The setting is needed for special reset conditions.

The secondary operational zero-sequence voltages can be obtained by reading the residual voltage V_{Nsec} or the zero-sequence voltage V0_{sec} under the symmetrical components from the device or via DIGSI. In case you read the secondary residual voltage V_{Nsec}, you convert it to V0_{sec} with the Matching ratio Vph / VN parameter. Its setting is usually √3.

Recommendation:

- If the maximum operational zero-sequence voltage is known, set the threshold to 1.2 V0_{op,max}
- If the maximum operational zero-sequence voltage is unknow and cannot be determined for any reason, please keep the default of 3V

Example:
Maximum operational secondary residual voltage reading: \( V_{N_{sec}} = 5.0 \text{ V} \)

Matching ratio \( V_{p_h} / V_{N} = \sqrt{3} \)

\[
V_{0_{sec}} = 5.000 \text{ V} \cdot \frac{\sqrt{3}}{3} = 2.887 \text{ V}
\]

Maximum operational \( V_0 = 2.887 \text{ V} \cdot 1.2 = 3.464 \text{ V} \)

### 3I0> threshold for pickup

In ring or meshed systems, you can use this parameter to reduce the number of ground-fault reporting devices. The parameter needs to be set according to the user experience on the specific network. For radial systems, normally you can keep the default value of 0 A which sets this parameter to inactive.

**Recommendation:** set this functionality inactive by keeping the default value of 0 A

### 3I0> threshold for operate, Operate delay, Dropout delay

These settings are not relevant since the operate functionality is not applied. Default settings can be applied.

### 6.1.2 Routing notes

We recommend the following routing for operational log (column O), fault log (column F) and Recorder. This routing allows reliable ground-fault clarification.

**Transient Ground Fault Function:**

![Signal list with recommended routing for the Transient Ground Fault Function](image)

**Function block General:**
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Figure 34  Signal list with recommended routing for the FB General

We recommend routing the signal **Pos. measuring window** into the fault recorder. This signal is essential for later ground-fault clarifications.

### 6.1.3  Further notes

**Avoiding floods of logs and recordings in case of intermittent ground faults**

The stage is fully immune against generating such floods during intermittent ground faults. No measures need to be taken.

**Avoiding floods of signals in case of intermittent ground faults**

The stage is fully immune against generating such floods during intermittent ground faults. No measures need to be taken.
7 V0 and 3I0 threshold considerations and examples

7.1 V0 Pickup threshold

In the following different approaches are described how the V0 setting value for a pickup or release threshold can be obtained.

A V0 threshold setting is derived for the network. The derived setting is identically for all feeders.

General V0 thresholds convention

All device V0 thresholds are set as zero-sequence voltage V0 according to definition. In case of full voltage displacement, the open-delta voltage Ven is 100 V for a typical transformer ratio. The equivalent secondary V0 voltage is then 100/√3 = 57.7 V.

Different approaches to obtain the threshold value are:

1. The user has historical experiences and good experiences with a V0 threshold value. The user reuses his previous threshold values. Please consider setting the threshold with relation to V0. You might have to divide your former setting value (if this was set with reference to Ven) by e.g. √3.

2. A typical V0> threshold value is applied. Typical values are 30%, 40%, or 50% of the full voltage displacement condition:
   - 30%: V0> threshold = 57.7 * 0.3 ≈ 17 V
   - 40%: V0> threshold = 57.7 * 0.4 ≈ 23 V
   - 50%: V0> threshold = 57.7 * 0.5 ≈ 29 V

3. The threshold is set according to the requirement to detect ground faults till a defined maximum ground fault resistance, please refer to the following chapter.

7.1.1 V0 Pickup threshold related to a defined ground fault resistance, resonant-grounded networks

In this chapter a well proven approximation is given how to derive the V0 threshold from the network data and the preset ground fault resistance:

\[ V_0 = v_{rel} \frac{V_{rated}}{\sqrt{3}} \]  
\[ v_{rel} = \frac{1}{\sqrt{1 + 2 \cdot \varepsilon \cdot d + \varepsilon^2 \cdot d^2 + \varepsilon^2 \cdot v^2}} \]  
\[ \varepsilon = \frac{\sqrt{3} \cdot R_F \cdot I_{CE}}{V_{rated}} \]

V0: Zero sequence voltage (as primary value) for a defined network and a preset ground fault resistance and
V_{rated}: rated primary network voltage, in V primary (value given)
Directional ground fault detection in resonant-grounded or isolated networks

\( V_{\text{rel}} \): factor that describes the reduction of the full displacement voltage in dependency of the ground fault resistance (calculated from given / known values)

\( \varepsilon \): aux. quantity (calculated from given / known values)

\( d \): Damping \( d \), in % (value known, or can be taken from the arc-suppression coil controller)

\( \nu \): detuning degree, in % (value given)

(for over-compensation: positive value, for under-overcompensation: negative value)

\( R_F \): Ground fault resistance till which a ground fault shall be detected, in \( \Omega \) (preset value)

\( I_{CE} \): Capitative ground current of the network (value given)

**Threshold calculation example acc. sample network S1 (radial, resonant-grounded)**

In the following a \( V_0 \) threshold calculation example is given for sample network S1, described in chapter 7.3.

- Ground faults up to a maximum ground fault resistance of 3k\( \Omega \) shall be detected:
  - \( R_F = 3k\Omega \)
- Network data is taken from the sample network S1:
  - \( I_{CE} = 300 \, A \)
  - \( V_{\text{rated}} = 20 \, kV \)
  - \( d = 3.1 \% \)
  - \( \nu = 4 \% \)
- Voltage transformer ratio: \( r = 20 \, kV / 100 \, V = 200 \)

\[ \varepsilon = \frac{\sqrt{3} \cdot 3000 \, \Omega \cdot 300 \, A}{20000 \, V} \approx 78 \]

\[ V_{\text{rel}} = \frac{1}{\sqrt{1 + 2 \cdot 78 \cdot 0.031 + 78^2 \cdot 0.031^2 + 78^2 \cdot 0.04^2}} = \frac{1}{\sqrt{1 + 4.836 + 5.847 + 9.734}} = 0.216 \]

\[ V_0 = 0.216 \frac{20000}{\sqrt{3}} \, V = 2494 \, V \]

\[ V_{0 \text{sec}} = 2494 \, V / r = 2494 \, V / 200 = 12.47 \, V \]

Between theoretically calculated and real setting value we consider a safety margin of approx. 20\%, resulting in the following threshold setting:

\( V_0 \) threshold = 10 V

For the detection of ground faults up to 3k\( \Omega \) ground fault resistance \( V_0 \) pickup or release thresholds should be set to 10 V (secondary).

**7.1.2 V0 Pickup threshold related to a defined ground fault resistance, isolated networks**

For isolated networks the consideration according to chapter 7.1.1 can be simplified.

Referencing Equation 2:

\[ V_{\text{rel}} = \frac{1}{\sqrt{1 + 2 \cdot \varepsilon \cdot d + \varepsilon^2 \cdot d^2 + \varepsilon^2 \cdot \nu^2}} \]
For isolated networks:

d: Damping d is set to 0, because there is no damping through the arc-suppression coil and the remaining ohmic damping is neglectable.

ν: detuning degree ν is set to -1 (=-100%) because no compensation is present

This simplifies Equation 2 to:

\[
V_{\text{rel}} = \frac{1}{\sqrt{1 + \varepsilon^2}} \quad \text{Equation 4}
\]

with

\[
\varepsilon = \frac{\sqrt{3} \cdot R_F \cdot I_{CE}}{V_{\text{rated}}}
\]

\( V_{\text{rel}} \): factor that describes the reduction of the full displacement voltage in dependency of the ground fault resistance (calculated form given / known values)

\( \varepsilon \): aux. quantity (calculated from given / known values)

\( R_F \): Ground fault resistance till which a ground fault shall be detected, in Ω (preset value)

\( I_{CE} \): Capitative ground current of the network (value given)

\( V_{\text{rated}} \): rated primary network voltage, in V primary (value given)

With factor \( V_{\text{rel}} \) the zero-sequence voltage can be calculated in dependency from the ground fault resistance as following:

\[
V_0 = V_{\text{rel}} \frac{V_{\text{rated}}}{\sqrt{3}}
\]

\( V_0 \): Zero sequence voltage (as primary value) for a defined network and a preset ground fault resistance \( R_F \)

Threshold calculation example

In the following a \( V_0 \) threshold calculation example is given:

- Ground faults up to a maximum ground fault resistance of 300 Ω shall be detected:
  - \( R_F = 300 \) Ω
- Network data:
  - \( I_{CE} = 200 \) A
  - \( V_{\text{rated}} = 20 \) kV
- Voltage transformer ratio: \( r = 20 \) kV / 100 V = 200

\[
\varepsilon = \frac{\sqrt{3} \cdot 300 \Omega \cdot 200 \text{ A}}{20000 \text{ V}} \approx 5.2
\]

\[
v_{\text{rel}} = \frac{1}{\sqrt{1 + 5.2^2}} = \frac{1}{\sqrt{1 + 27}} \approx 0.189
\]

\[
V_0 = 0.189 \frac{20000 \text{ V}}{\sqrt{3}} = 2182 \text{ V}
\]

\( V_{\text{0 sec}} = 2182 \text{ V} / r = 2182 \text{ V} / 200 = 10.9 \) V
Between theoretically calculated and real setting value we consider a safety margin of approx. 20%, resulting in the following threshold setting:

\[ V_0 \text{ threshold} = 8.7 \text{ V} \]

For the detection of ground faults up to 300 Ω ground fault resistance V0 pickup or release thresholds should be set to 8.7 V (secondary).

### 7.1.3 V0 Pickup threshold consideration for intermittent ground faults

From network simulations and real field case recordings it can be noted that frequent ground-fault re-striking significantly increases the zero-sequence voltage V0, but not completely to the same level as for a permanent ground fault. This is also true for high-ohmic ground faults. In this regard Figure 35 shows the VN voltage rise during the re-striking period for a very high ohmic ground fault (7..18 kΩ).

**Recommendation:** The V0 pickup threshold consideration made in chapter 7.1.1 are true for permanent ground faults. Since V0 for intermittent ground faults does not fully reach the V0 level for permanent faults we propose to set the V0 threshold to 60% of the V0 value derived in chapter 7.1.1, if the function should detect intermittent ground faults and if ground-fault to a defined ground-fault resistance should be detected.

**Example:**

- V0sec value for permanent ground-faults up to 3kΩ ground fault resistance, according to chapter 7.1.1:
  \[ V_{0\text{sec}} = 12.47 \text{ V} \]
- V0 threshold for intermittent ground faults: \[ V_0 \text{ threshold} = 12.47 \text{ V} \cdot 0.6 = 7.5 \text{ V} \]

![Figure 35](image)

**Figure 35** very high-ohmic intermittent ground fault (7..18 kΩ)

### 7.2 3I0 thresholds for radial networks

In the following different approaches are described how a 3I0 setting value for a pickup or release threshold can be obtained (for radial networks).

3I0 threshold settings related to the total 3I0 (active and reactive current) must be derived for each network feeder individually. Each feeder requires a specific setting. Most 3I0 function thresholds relate to the total 3I0. For the \( \text{Cos}\phi \) function additionally one threshold relates to the active (ohmic) 3I0 component 3I0active. The active (ohmic) 3I0...
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Component \(3I_{0active}\) is feeder independent. The threshold can be set identically for all feeders. For both values (\(3I_{0total}\) and \(3I_{0active}\)) considerations are made in the following.

Different approaches to obtain the threshold value are:

1. The user has historical experiences and good experiences with \(3I_0\) threshold values per feeder. The user reuses his previous threshold values.

2. A "rule of thumb" setting value approach can be applied. This approach is simple, requires only very little calculation efforts and gives good detection results, when no detection up to a defined ground fault resistance is required. Please refer to chapter 7.2.1.

3. The threshold is set according to the requirement to detect ground faults till a defined maximum ground fault resistance, please refer to the chapter 7.2.2.

### 7.2.1 \(3I_{0active}\) threshold related to “rule of thumb” approach, resonant-grounded networks

In this chapter a simple rule of thumb approach is given for the \(3I_{0active}\) determination, which is required for the \(\cos \phi\) stage. \(3I_{0active}\) is feeder independent.

The active ground current \(3I_{0active}\) can be determined via the following formula:

\[
3I_{0active} = d \cdot I_{CE}
\]

**Equation 5**

- \(3I_{0active}\): Active zero sequence current (as primary value) for zero ground fault resistance \(R_f\), this value is identical for all feeders of the network
- \(d\): Damping d, in % (value known, or can be taken from the arc-suppression coil controller)
- \(I_{CE}\): Capitative ground current of the network (value given)

The rule of thumb is to set the respective threshold value in a range between 25% to 50% of the active ground current \(3I_{0active}\).

\[3I_{0active\ threshold} = 0.25 ... 0.5 \cdot 3I_{0active}, \ e.g. \ 0.3 \cdot 3I_{0active}\]

**Threshold calculation example acc. sample network S1 (radial, resonant-grounded)**

In the following a \(3I_{0active}\) threshold calculation example is given for sample network S1, described in chapter 7.3.

- **Network data is taken from the sample network S1:**
  - \(I_{CE} = 300 \text{ A}\)
  - \(d = 3.1 \%\)
- **Current transformer ratio (core balance CT):** \(r = 80 \text{ A} / 1 \text{ A} = 80\)

\[
3I_{0active} = d \cdot I_{CE} = 0.031 \cdot 300 \text{ A} = 9.3 \text{ A}
\]

\[
3I_{0active/sec} = \frac{9.34 \text{ A}}{r} = \frac{9.34 \text{ A}}{80} \approx 116 \text{ mA}
\]

\[3I_{0active\ threshold} = 0.3 \cdot 3I_{0active} = 0.3 \cdot 116 \text{ mA} = 35 \text{ mA}\]

Parameter **Min. polar.\(3I_{0}\) for dir.det.** of the \(\cos \phi\) stage is set to 35 mA for all feeders in this network.
7.2.2 3I0 threshold related to a defined ground fault resistance, resonant-grounded networks

In this chapter a well proven approximation is given how to derive the 3I0 thresholds from the network data and the preset ground fault resistance, for resonant-grounded networks:

\[ 3I_{0\text{, total, }fd} = \sqrt{(3I_{0\text{, active}})^2 + (3I_{0\text{, reactive}})^2} \]  \hspace{1cm} \text{Equation 6}

\[ 3I_{0\text{, active}} = \nu \cdot d \cdot I_{CE} \]  \hspace{1cm} \text{Equation 7}

\[ 3I_{0\text{, reactive}} = \nu \cdot (\nu \cdot I_{CE} + I_{CE,feeder}) \]  \hspace{1cm} \text{Equation 8}

3I_{0\text{, total, }fd}: \text{ Total zero sequence current (as primary value) for a preset ground fault resistance } R_f, \text{ per feeder}

3I_{0\text{, active}}: \text{ Active zero sequence current (as primary value) for a preset ground fault resistance } R_f, \text{ this value is identical for all feeders of the network}

3I_{0\text{, reactive}}: \text{ Reactive zero sequence current (as primary value) for a preset ground fault resistance } R_f, \text{ per feeder}

I_{CE,feeder}: \text{ Capitative ground current of a network feeder (value given)}

\nu: \text{ factor that describes the reduction of the full displacement voltage in dependency of the ground fault resistance (calculated form given / known values), acc. to Equation 2 (in chapter 7.1.1)}

\varepsilon: \text{ aux. quantity (calculated form given / known values), acc. to Equation 3 (in chapter 7.1.1)}

d: \text{ Damping } d, \text{ in } \% (\text{value known, or can be taken from the arc-suppression coil controller)}

\nu: \text{ detuning degree, in } \% (\text{value given})

\text{(for over-compensation: positive value, for under-overcompensation: negative value)}

R_f: \text{ Ground fault resistance till which a ground fault shall be detected, in } \Omega (\text{preset value})

I_{CE}: \text{ Capitative ground current of the network (value given)}

V_{rated}: \text{ rated primary network voltage, in } V \text{ primary (value given)}

Threshold calculation example acc. sample network S1 (radial, resonant-grounded)

In the following a 3I0 threshold calculation example is given for sample network S1, described in chapter 7.3. The example is made for feeder F3:

- Ground faults up to a maximum ground fault resistance of 3kΩ shall be detected:
  - \( R_f = 3kΩ \)
- Network data is taken from the sample network S1:
  - \( I_{CE} = 300 \text{ A} \)
  - \( I_{CE,feeder F3} = 28 \text{ A} \)
  - \( V_{rated} = 20 \text{ kV} \)
  - \( d = 3.1 \% \)
  - \( \nu = 4 \% \)
- Current transformer ratio (core balance CT): \( r = 80 \text{ A} / 1\text{A} = 80 \)

\[ \varepsilon = \frac{\sqrt{3} \cdot 3000 \Omega \cdot 300 \text{ A}}{20000 \text{ V}} \approx 78 \]
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\[ v_{rel} = \frac{1}{\sqrt{1 + 2 \cdot 78 \cdot 0.031 + 78^2 \cdot 0.031^2 + 78^2 \cdot 0.04^2}} = \frac{1}{\sqrt{1 + 4.836 + 5.847 + 9.734}} = 0.216 \]

\[ 3I_0_{active} = 0.216 \cdot 0.031 \cdot 300 \, A = 2.01 \, A \]
\[ 3I_0_{reactive} = 0.216 \cdot (0.04 \cdot 300 \, A + 28 \, A) \approx 8.6 \, A \]
\[ 3I_0_{total,fd} = \sqrt{2.01^2 + 8.6^2} \cdot A \approx 8.8 \, A \]

\[ 3I_0_{total,fd,sec.} = \frac{8.8}{r} \cdot A = \frac{8.8}{80} \cdot A = 110 \, mA \]
\[ 3I_0_{active,sec.} = \frac{2.01}{r} \cdot A = \frac{2.01}{80} \cdot A = 25.1 \, mA \]

The threshold values are set approx. 20% below the calculated values, which serves as safety margin:

- 3I_0\_total,fd F3 threshold = 110 mA \cdot 0.8 \approx 88 mA
- 3I_0\_active threshold = 25.1 mA \cdot 0.8 \approx 20 mA  \text{(required in CosPhi function)}

For the detection of ground faults in feeder F3 up to 3kΩ ground fault resistance the 3I_0\_total thresholds should be set to 88 mA (secondary). The 3I_0\_active threshold which is additionally required in the CosPhi function should be set to 20 mA (secondary).

7.2.3 3I_0 threshold related to a defined ground fault resistance, isolated networks

In this chapter a well proven approximation is given how to derive the 3I_0 thresholds from the network data and the preset ground fault resistance, for isolated networks:

\[ 3I_0_{cap,fd} = v_{rel} \cdot (I_{CE} - I_{CE,feeder}) \]  \text{Equation 9}
\[ 3I_0_{total,fd} \approx 3I_0_{cap,fd} \]  \text{Equation 10}

Capacitive and total sequence current per feeder are approximately the same, since the active zero-sequence current is neglectable for an isolated network

3I_0\_cap,fd: Capacitive zero sequence current (as primary value) for a preset ground fault resistance Rr, per feeder
3I_0\_total,fd: Total zero sequence current (as primary value) for a preset ground fault resistance Rr, per feeder
I_{CE}: Capitative ground current of the network (value given)
I_{CE,feeder}: Capitative ground current of a network feeder (value given)

with \( v_{rel} \) for an isolated network according to Equation 4 (from chapter 7.1.2)

\[ v_{rel} = \frac{1}{\sqrt{1 + \varepsilon^2}} \]

with
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\[ \varepsilon = \frac{\sqrt{3} \cdot R_F \cdot I_{CE}}{V_{rated}} \]

- \( \varepsilon \): aux. quantity (calculated from given / known values)
- \( R_F \): Ground fault resistance till which a ground fault shall be detected, in \( \Omega \) (preset value)
- \( I_{CE} \): Capitative ground current of the network (value given)
- \( V_{rated} \): rated primary network voltage, in V primary (value given)

**Threshold calculation example**

In the following a 3I0 threshold calculation example is given:

- Ground faults up to a maximum ground fault resistance of 300 \( \Omega \) shall be detected:
  - \( R_F = 300 \Omega \)
- Network data:
  - \( I_{CE} = 200 \, A \)
  - \( I_{CE,feeder} = 40 \, A \)
  - \( V_{rated} = 20 \, kV \)
- Current transformer ratio (core balance CT): \( r = 80 \, A / 1A = 80 \)

\[ \varepsilon = \frac{\sqrt{3} \cdot 300 \Omega \cdot 200 \, A}{20000 \, V} \approx 5.2 \]

\[ v_{rel} = \frac{1}{\sqrt{1 + 5.2^2}} = 0.189 \]

\[ 3I_{0,\text{cap},fd} = 0.189 \cdot (200 \, A - 40 \, A) \approx 30 \, A \]
\[ 3I_{0,\text{total},fd} \approx 30 \, A \]

\[ 3I_{0,\text{cap},fd,sec.} = 3I_{0,\text{total},fd,sec.} = \frac{30 \, A}{80} = 375 \, mA \]

The threshold values are set approx. 20% below the calculated values, which serves as safety margin:

\[ \Rightarrow 3I_{0,\text{total},fd} \text{ threshold } = 375 \, mA \cdot 0.8 = 300 \, mA \]

For the detection of ground faults up to 300 \( \Omega \) ground fault resistance in this feeder the 3I0 threshold should be set to 300 mA (secondary). The 3I0capactive threshold (parameter **Min.polar.3I0> for dir.det.**), which is additionally required in the SinPhi function, should be set to the same value (300 mA).
7.2.4 3I0 threshold related to a defined ground fault resistance consideration for intermittent ground faults

**Recommendation:** The 3I0 threshold considerations made in chapter 7.2.2 relate to a permanent ground-fault. During an intermittent ground fault, the 3I0 ground fault current level will not fully reach the fault current level for a permanent ground fault. Therefore, we propose to set the 3I0 threshold to 60% of the value derived in chapter 7.2.2, if the function should detect intermittent ground faults and if ground-fault to a defined ground-fault resistance should be detected.

**Example:**
- 3I0 value for permanent ground-faults up to 3kΩ ground fault resistance, according chapter 7.2.2:
  \[3I0_{\text{total,fd,sec.}} = 110 \text{ mA}\]
- 3I0 threshold for intermittent ground faults: \[3I0_{\text{threshold}} = 110 \text{ mA} \times 0.6 = 66 \text{ mA}\]

7.3 Sample network S1: radial, resonant-grounded

The following figure shows a sample network for a radial, resonant-grounded 20 kV network, which serves for the explanation of setting recommendations given the "setting notes" chapters for the described functions.

This sample network consists of:
- radial pure overhead line feeders with different lengths (F1, F2)
- radial mixed overhead and cable feeders with similar length (F3, F4)
- radial pure cable feeders cable feeder with different lengths (F5, F6, F7, F8)
- closed cable ring (F9, F10)

**Network data:**
- Rated network voltage, \(V_{\text{rated}} = 20 \text{ kV}\)
- Capitative ground current of the network, \(I_{\text{CE}} = 300 \text{ A}\)
- 4% overcompensation = 12 A, Arc-suppression coil current \(I_{\text{ASC}} = 312 \text{ A}\)
- Ohmic coil losses = 6 A
- Damping \(d = 3.1\%\) (The damping should be known. E.g. it is provided as measuring value by the arc-suppression coil controller.)
- Active ground-current component \(I_a = 9.3 \text{ A} = d \times I_{\text{CE}}\)
- Operational \(V_0 = 0.8 \text{ V} \) (\(V_0\) under fault free condition)
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Figure 36  Sample network, resonant-grounded network
7.4 CFC proposal for a Minimum operate delay related to the function “Dir. Intermittent ground fault protection”

The function Dir. Intermittent ground fault protection (DIGFP) will mostly be applied in the operating mode Counter. In this mode the function trips if a defined number of restrikes were detected. In this mode the tripping time is not defined and depends strongly on the individual intermittent fault characteristic and its re-striking frequency. Fast re-striking causes fast tripping, slow re-striking causes slower tripping.

It could be required to ensure a minimum operate delay time to avoid very fast tripping. For this purpose, the CFC logic proposal acc. Figure 37 can serve. The CFC has been tested and it operates as designed.

**Note:** With firmware version V8.3 and greater (starting in 08/2020) the minimum operate delay time is introduced as a new function parameter and can be set directly in the function Dir. Intermittent ground fault protection. No CFC will be required.

Steps prior to implementing the CFC

Before the CFC logic is implanted the following steps should / must be carried out.

1. Stage setting Operate & flt.rec. blocked must be set to yes.
   This is required to block the standard stage operate signal, which otherwise could reset the stage too early. However, this prevents form automatic fault recording. So now the fault recording must be started manually (refer to the device manual for further information).

2. Configure an External trip stage
   The standard stage operate signal is blocked. The trigger for the new delayed “operate” (trip) signal will be generated by the CFC. The CFC output will trigger the External trip stage. By this the delayed operate signal is fed again into the normal trip interface to the CB.

3. Configure the minimum operate delay time (which is executed in the CFC) as a standard parameter
   Refer to chapter 7.4.1 for such a configuration

Implementing the CFC

When creating the CFC the task level can be selected as Event-triggered., refer to the following screen shot:
Logics description of the CFC:

Figure 37  CFC logic for minimum operate delay

Three signals of the DIGFP stage are inputs to the CFC:

- **Pickup:**
  The pickup sets the flipflop (FF) and start the timer Minimum operate delay. By means of the FF the timer is kept running during the intermittent ground fault, while the pickup signal could also drop out.

- **Pulse no. reached:**
  If the signal Pulse no. reached is given and timer Minimum operate delay has expired the tripping condition is fulfilled. A 100 ms pulse is generated to trigger the External trip function. After 100 ms the >External trip signal will drop put.

- **Reset time running:**
  The expiration of the reset time resets the DIGFP function, and as well the SR-FF of the CFC chart.

Timers:

- **Minimum operate delay timer:**
  The timer should be of the type TON.
  The time delay is defined via the PT input in the unit "ms", if e.g. set to 2000 the time delay is 2 s. The PT input is set via parameter Min operate delay.value.

- **Trip duration:**
  The timer should be of the type TP.
  The time delay is defined via the PT input in the unit "ms", if e.g. set to 100 the generated pulse duration is 100 ms.
7.4.1 CFC Timer setting as normal setting

A CFC delay timer setting can be defined in a way that it can be changed in the standard way via the DIGSI seeing editor or via the device HMI, without the need of changing and compiling the CFC chart. In the following a description for such a configuration is provided, by the example for the function 67Ns Dir.sens GFP1. steps and status:

1. open in the DIGSI lib the User-defined function
2. Drag a function block Chart setting integer from the lib and drop it into the function 67Ns Dir.sens GFP1
3. After that you will find this FB/setting in setting editor at the bottom of the function 67Ns Dir.sens GFP1
4. Set the required delay time in ms, e.g. 1000 [ms] for 1 s delay.
   (the unit is determined by the respective CFC block TON which is a timer with a resolution in ms)
5. Open (or create) the CFC in which the setting shall be applied
6. With opening the CFC the right-hand side DIGSI editor should automatically show the Signals task card
7. Under Signals open the function group and the function 67Ns Dir.sens GFP1, there you will find the new FB/setting
8. Drag the Setting value from the list and drop on the PT input of the TON timer element.
9. Now you can change the TON timer value via this **Setting value** in standard DIGSI setting editor or the device HMI.